$= \begin{bmatrix} \frac{1}{2}x^2 - \frac{2}{2}x^2 \end{bmatrix}_{-1}^{-1} - \begin{bmatrix} \frac{1}{2}x^2 - \frac{2}{2}x^2 \end{bmatrix}_{0}^{-1} - \begin{bmatrix} \frac{1}{2}x^2$

Use of Unstressed Strands for Connections of Precast Concrete Members

⁶⁶Use of Unstressed Strands for Connections of Precast Concrete Members" by Xiao Liang and Sri Sritharan, which appeared in the May–June 2021 issue of *PCI Journal*, includes both experimental and analytical programs to explore the bond behavior and overall performance of unstressed strands for seismic applications in positive moment connections of precast concrete girders. Background information was provided on the differences in bond behavior between unstressed and prestressed strand, including a discussion of the Hoyer effect. In addition, work by Salmons and McCrate¹ and Noppakunwijai et al.² was referenced.

The issue of bond between prestressing steel and concrete has received a lot of research attention in the past 30 years. In many of these studies, the bond properties of strands in concrete were found to vary widely, partly due to differences in concrete properties but also due to variable surface residues left on strands during manufacturing. In our opinion, any experimental test program that studies strand bond should at least characterize the bond properties of the strand according to ASTM A1081.³ We did not see that this was done for this project. It also would have been appropriate, in our opinion, to fabricate and test the same cylindrical test specimens as ASTM A1081 using the grout mixture and the concrete member mixture. Alternatively, a strand bond qualification test in accordance with Peterman⁴ would be appropriate.

The authors are to be congratulated for adding the variable of cyclic loading to the strand bond issue, showing that strand bond degrades under high cyclic interface stresses.

We believe that there are a number of other relevant and important studies that are not mentioned in this paper that further discuss the bond behavior of unstressed and stressed strand in concrete and would be beneficial to readers. These include experimental testing by Moustafa,⁵ Moustafa pullout tests (large block pullout tests) by Logan,⁶ North American Strand Producers (NASP) strand bond round robin testing conducted by Russell et. al.,⁷⁻¹⁰ National Cooperative Highway Research Project (NCHRP) 603 report by Russell and Ramirez,¹¹ NCHRP 621 report by Osborn et al.,¹² the Kansas State University report by Polydorou et al.,¹³ bond testing of stressed strand by Naito et al.,¹⁴ and the due diligence report by Hawkins and Ramirez that summarize the results of these many studies.¹⁵ There is also an ongoing PCI project on experimental testing of prestressing strand lifting loops by Chhetri et al.¹⁶

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Authors' response

The writers would like to thank the discussers, Osborn and Chicchi, for their special interest in the original paper. Their comments and wealth of suggested references are greatly appreciated.

The study presented in the original paper was motivated to establish cost-effective and easily implementable positive moment connections between precast concrete bridge girders and bent caps, making the use of precast concrete girders in seismic regions cost competitive to cast-in-place construction. In this effort, unstressed strands extending from the ends of precast concrete girders are used as the connecting reinforcement.¹ The writers agree with the discussers that the bond of strands is influenced by many factors, which has been shown in many studies, including those that the discussers cited. The writers did not perform bond tests in accordance with ASTM A1081² because the width of the bent cap mainly determined the anchorage length in our tests. Furthermore, the intent of the tests with straight ends was to determine the maximum force that the strand can develop and measure the corresponding slip as a function of the force. With this information, we were able to determine whether the provided strand embedment length was adequate for the particular connection demand and the required capacity of a supplementary mechanical connection if needed to ensure full development of the unstressed strand.

Using a shorter embedment length for strands extending from precast concrete components such as girders and relying on a combination of bond stress and mechanical anchorage for developing the strand capacity also minimizes transportation and construction challenges. In this regard, the work done by Salmons and McCrate³ was valuable and was used as a reference. Considering that the objective of the original paper was to compare the responses of strands with different anchorage details and to determine the embedment length requirements for unstressed strands when used as connecting reinforcement between precast concrete members, the use of ASTM A1081 test was not deemed critical. Furthermore, our tests simulated the anchorage of the strands for our specific problem (anchoring the strands into a bent cap), creating a more realistic condition for the concrete with appropriate confinement effects. Finally, as presented in the original paper, we quantified the bond strength based on our test data, which is approximately five times the square root of the concrete compressive strength. This information would allow a designer to appropriately design the connection using unstressed strands and an appropriate supplemental mechanical anchorage. In cases where the strands



Figure 1. Use of unstressed strands in the positive seismic moment connections for precast concrete girders. Photo courtesy of Dorie Mellon, California Department of Transportation. can be anchored with a straight end, we expect the designer to follow the recommendations of the PCI Strand Bond Task Group⁴ or other appropriate guiding documents.

Although prestressing has been frequently used to establish connections between precast concrete members (for example, in Sritharan et al.⁵), unstressed strands in connections seldom have been used in practice. With a continuous emphasis on accelerated construction, we believe the use of the unstressed strands in connections, either as a new element or as an extension of pretensioned strands incorporated into precast concrete members, offers multiple advantages, as noted in the original paper. This is what we promoted in our study, which has begun to show deployments in field applications (Fig. 1). As suggested by the discussers, a more systematic study would provide many opportunities for the precast concrete industry to use unstressed strands for connecting prefabricated members in a variety of ways.

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