



# SEISMIC CONNECTIONS IN PREFABRICATED SUPERSTRUCTURES

---

Sri Sritharan  
Justin Vander Werff  
Rick Snyder

Iowa State University

**Nov. 17, 2011**

**Caltrans-PCMAC Precast Bridge Workshop**

# Outline

2

- Scope
- Use of I-girders with Inverted-tee bent Cap
- Prototype bridge
- Experimental investigation
- Conclusions

# Scope

3

- To understand the true seismic behavior of inverted tee cap-to-girder connections as currently used and the impact of such connections on the system response using both analytical and experimental means
- To mitigate the potential seismic hazard associated with these bridges

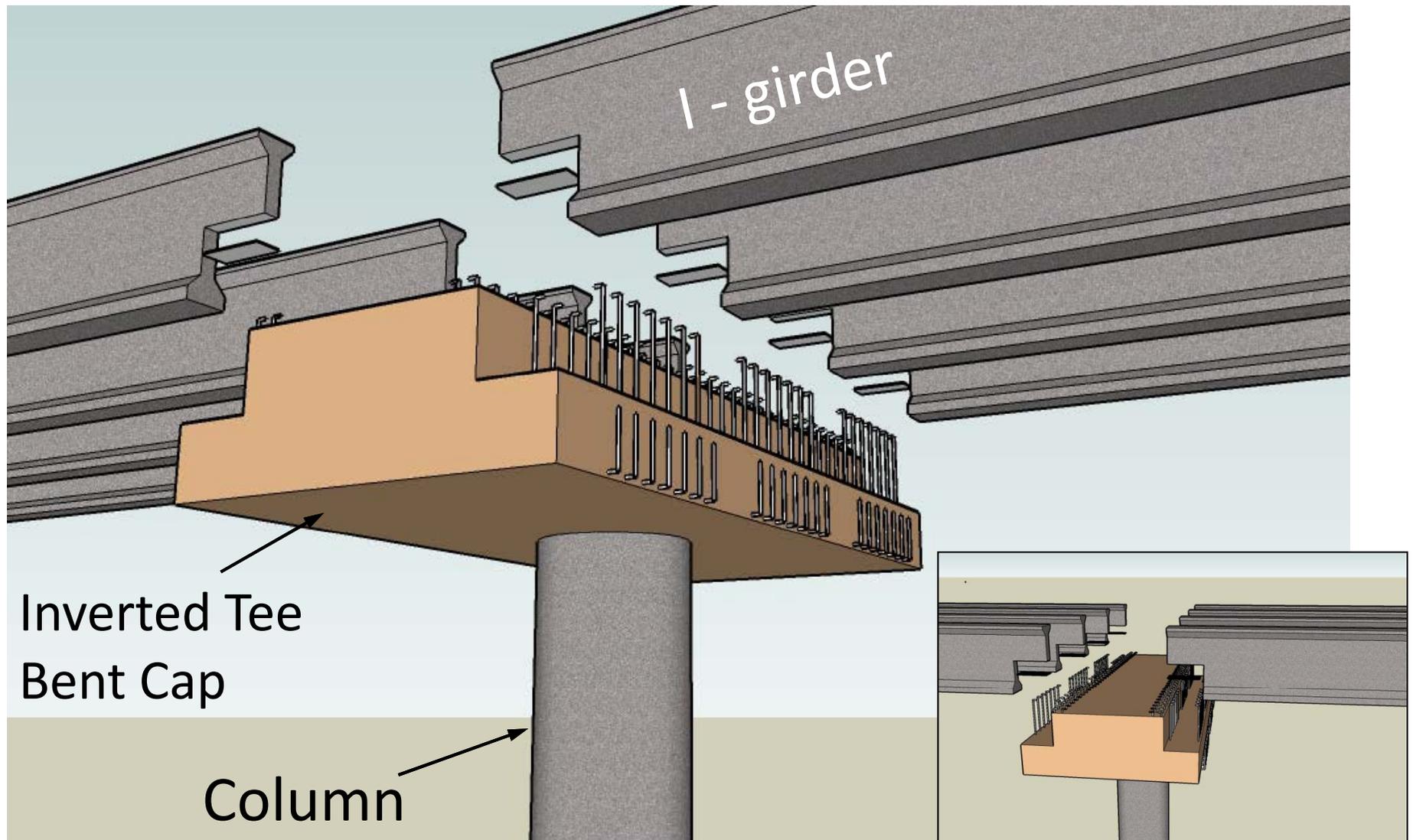
# Precast concrete girders in seismic regions

4

- Advantages of precast concrete
  - ▣ Shop construction (improved quality, reduced cost)
  - ▣ ABC (reduced field time, reduced traffic divergence, reduced noise and air pollution)
- However, not widely used in seismic regions
  - ▣ Lack of a proven design methodology
  - ▣ Lack of experimental validation of structural details/connections
  - ▣ I-girder/Inverted tee system is not cost effective

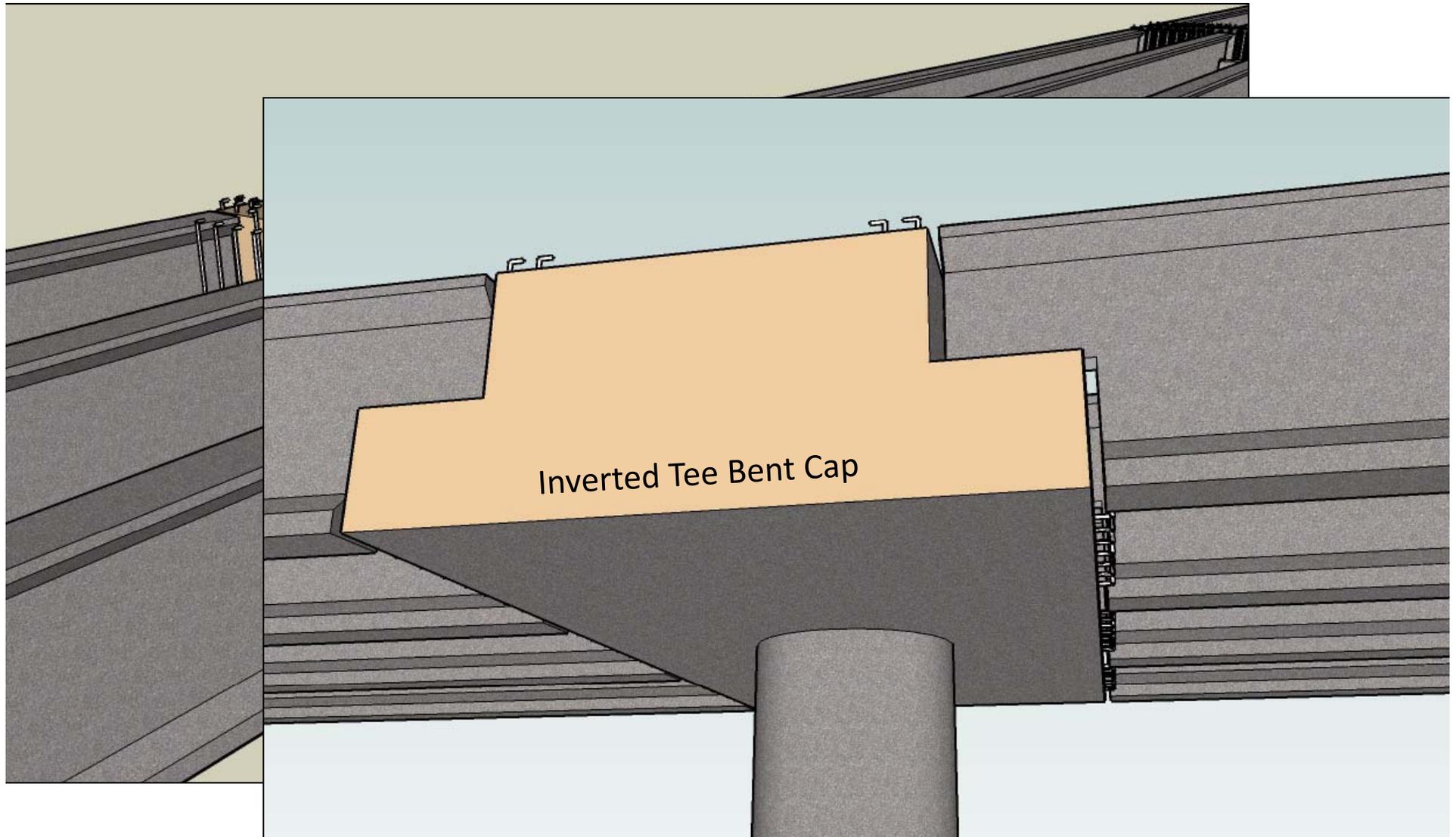
# I-girder with inverted-tee bent cap

5

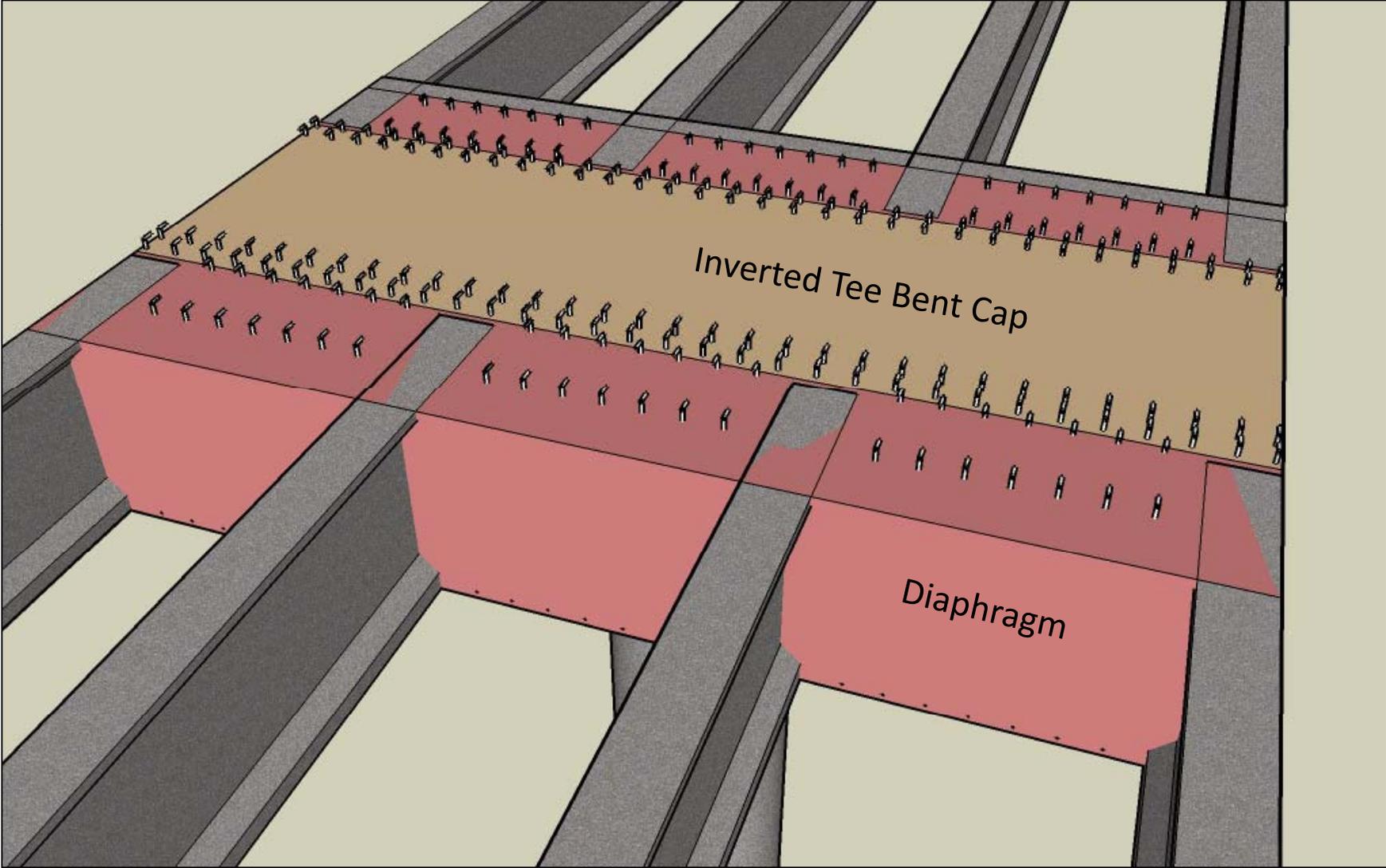


# Connection Details

6

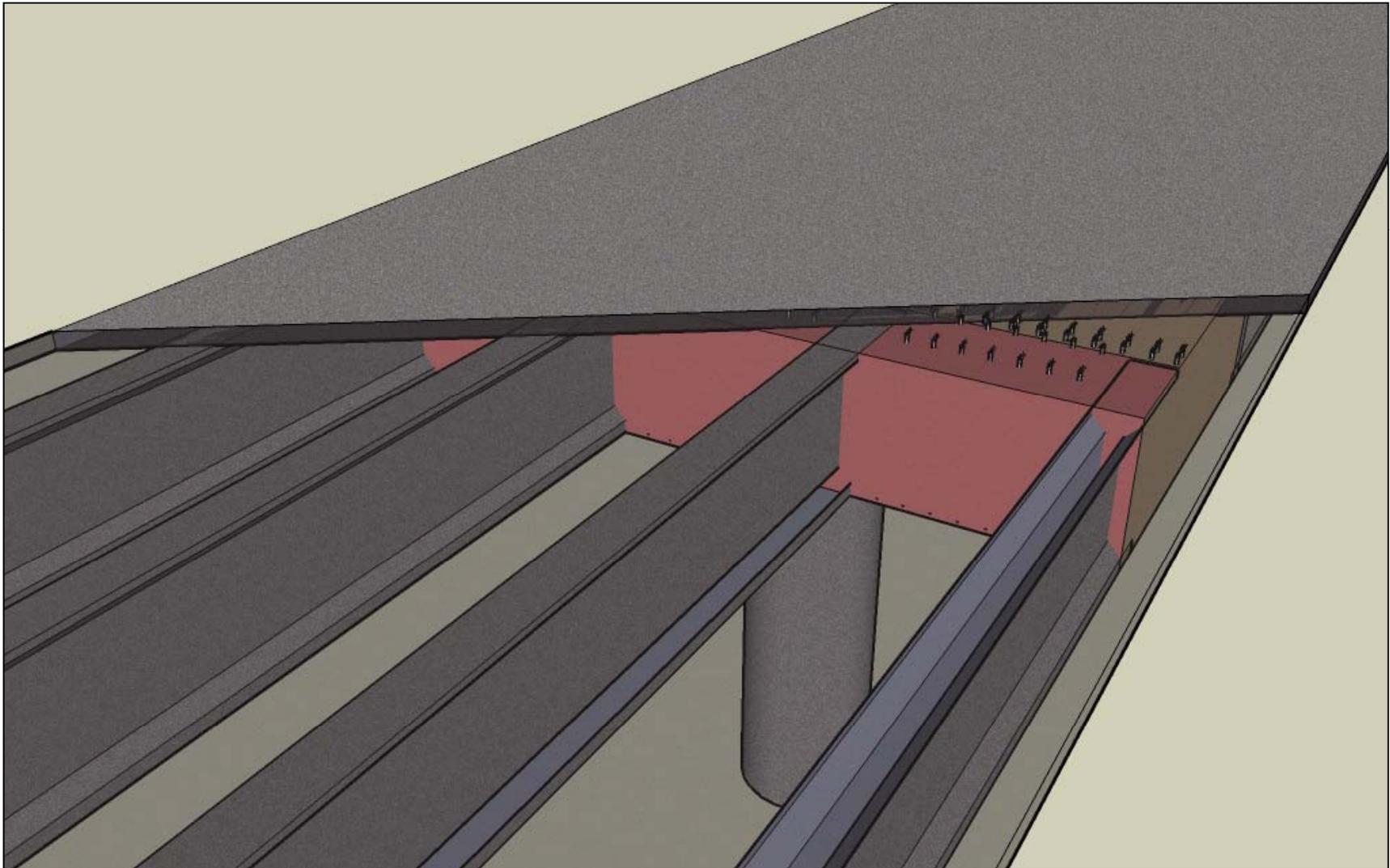


# Diaphragms Added



# Deck Added

8



# I-Girder/Inverted Tee Connection

9

- As-built condition
  - ▣ Assumed to degrade to a pin connection (due to lack of positive moment connection between the cap and girders)
  - ▣ A plastic hinge at the column top is not expected
  - ▣ Thus requiring a larger diameter columns and large foundations making it less cost effective in comparison to a cast-in-place alternative

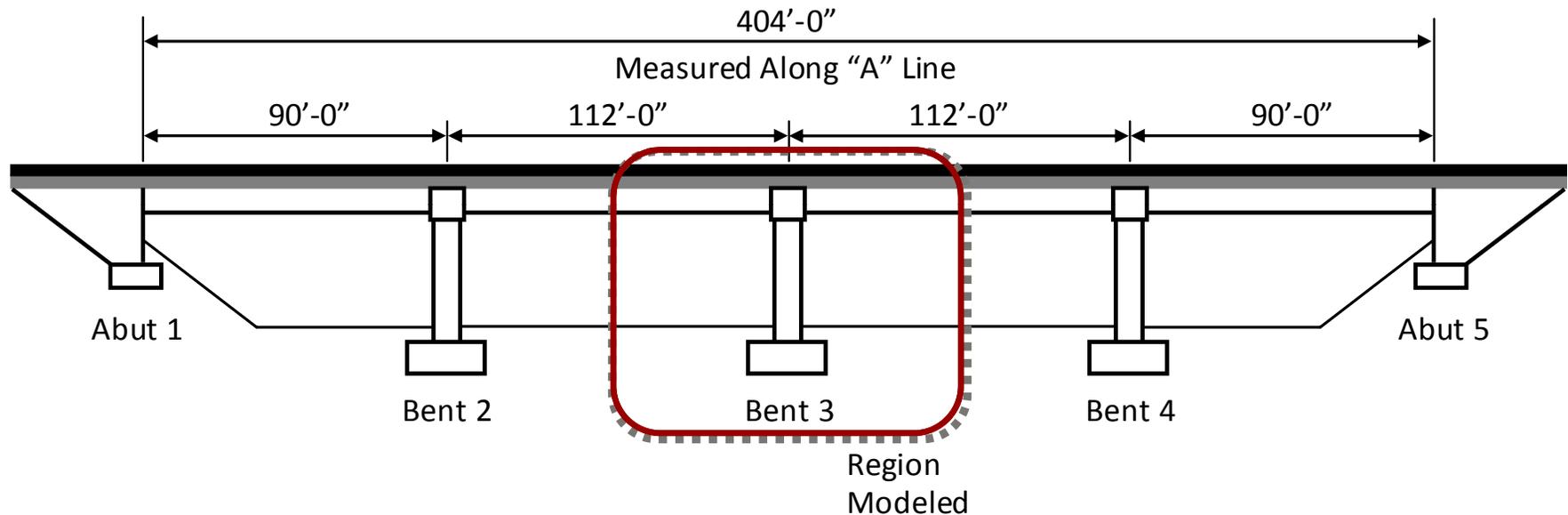
# I-Girder/Inverted Tee Connection

10

- Contribution of research
  - ▣ Analysis shows the as-built connection will act more like a fixed connection due to dowel bars going through the girders and integration of the connection using diaphragm and deck
  - ▣ An improved connection detail was explored as a possible detail for future bridge
  - ▣ After considering several options, the connection performance was improved by running grouted unstressed tendons in the bottom flange of the girders through the cap for the entire bridge length
  - ▣ Make this design option cost effective by allowing formation of a plastic hinge at the column top

# Prototype Bridge

11

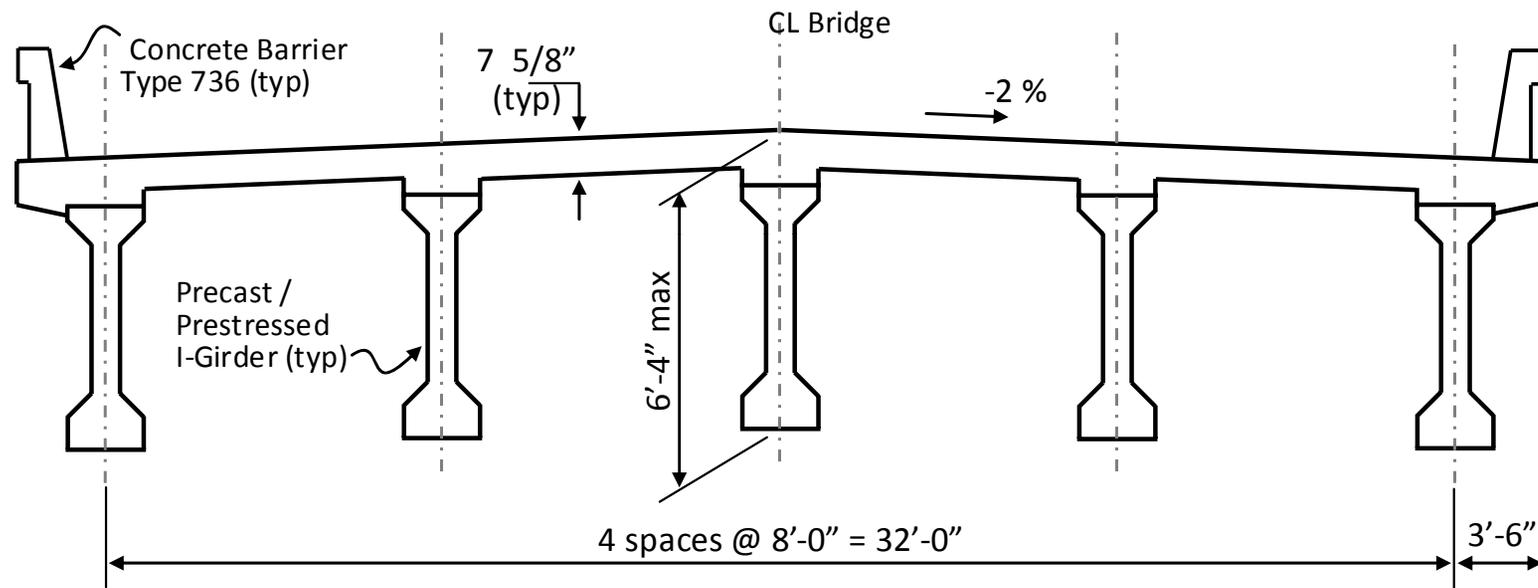


- Four spans (no skew)
- Total length = 123 m
- 34 m interior spans

- AASHTO LRFD with CA amendments
- Caltrans SDC
- Caltrans Bridge Design Aids

# Prototype Bridge - Section

12



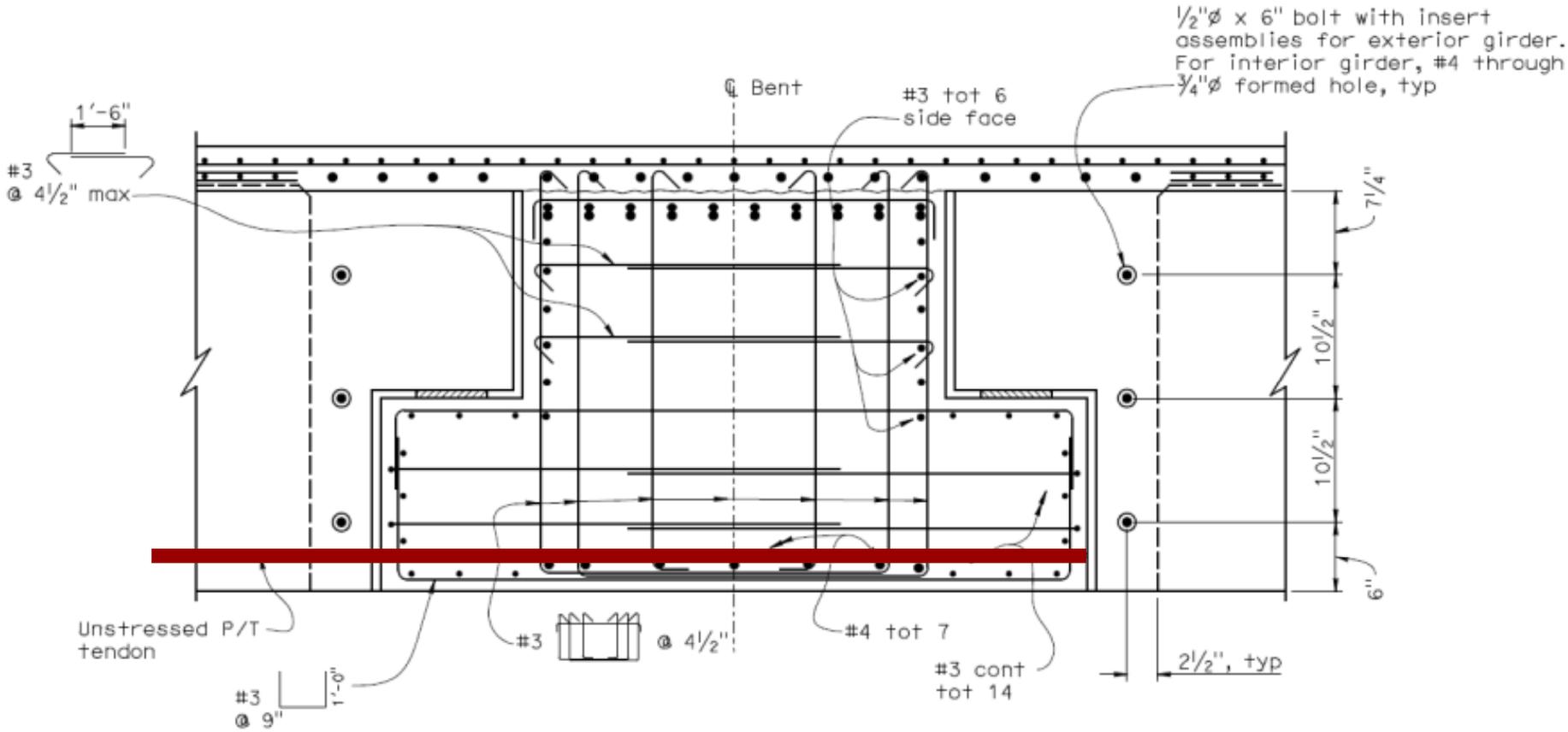
- Designed by PBS&J, verified by ISU
- SS Depth = 1.93 m
- D/S = 0.0565
- 5 precast I-Girders with 1.67 m depth
- CONSPAN for service load analysis/design

# Test Unit Configuration

13

- Center portion of prototype structure
- 50% dimensional scale
- Single column with inverted-tee cap beam
- Superstructure of five I-girders overlaid with deck
- As-built girder-to-cap connection on one side of cap beam and improved connection on other side

# Test Unit - Connection Details

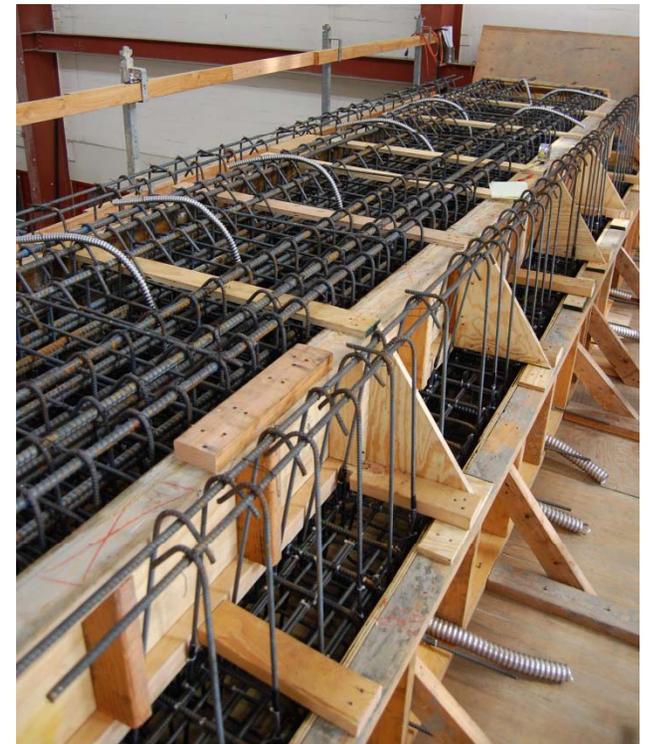


**Improved**

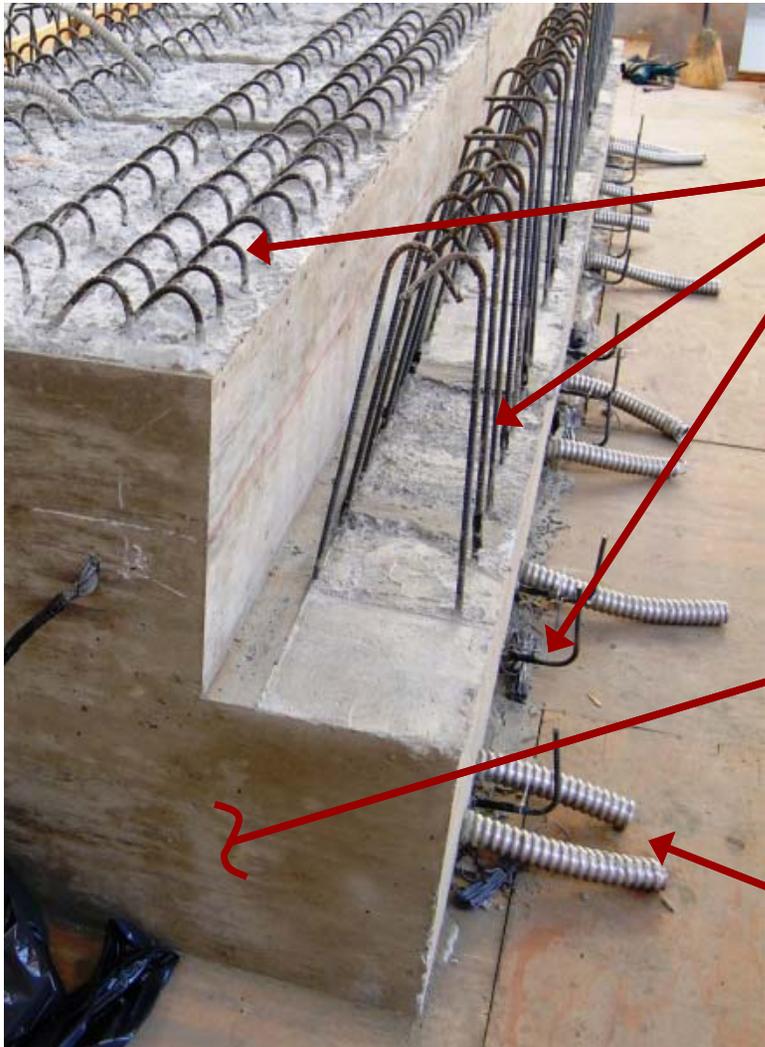
**As-built**

# Construction of Girders and Cap

15



# Inverted Tee



**Connection reinforcement**

**Inverted-tee cap beam**

**Strand ducts**

# Construction at UCSD Laboratory

17



# Test Phases

18

## □ Phase I Testing

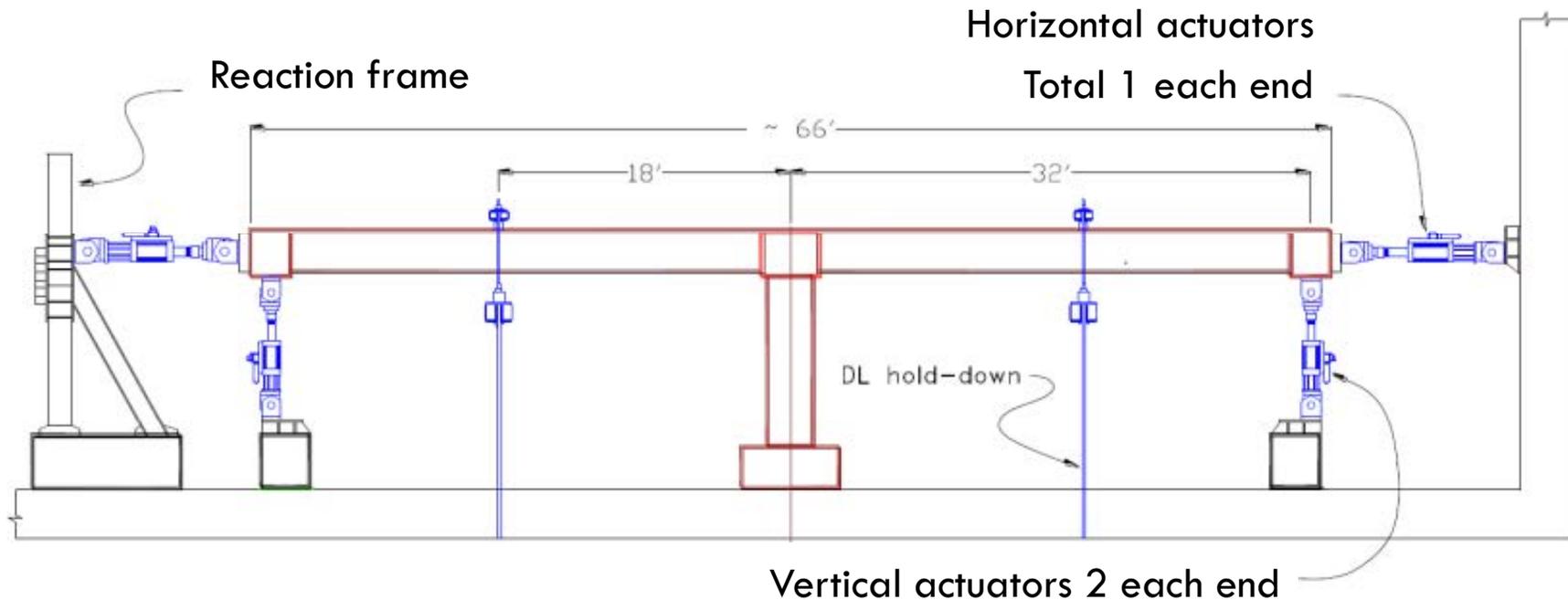
- Horizontal seismic testing
- Evaluate system performance
- Verify if both connections are adequate to form a plastic hinge at the column top

## □ Phase II Testing

- Vertical load/displacement
- Full exercise the girder-to-cap connections

# Phase I Configuration

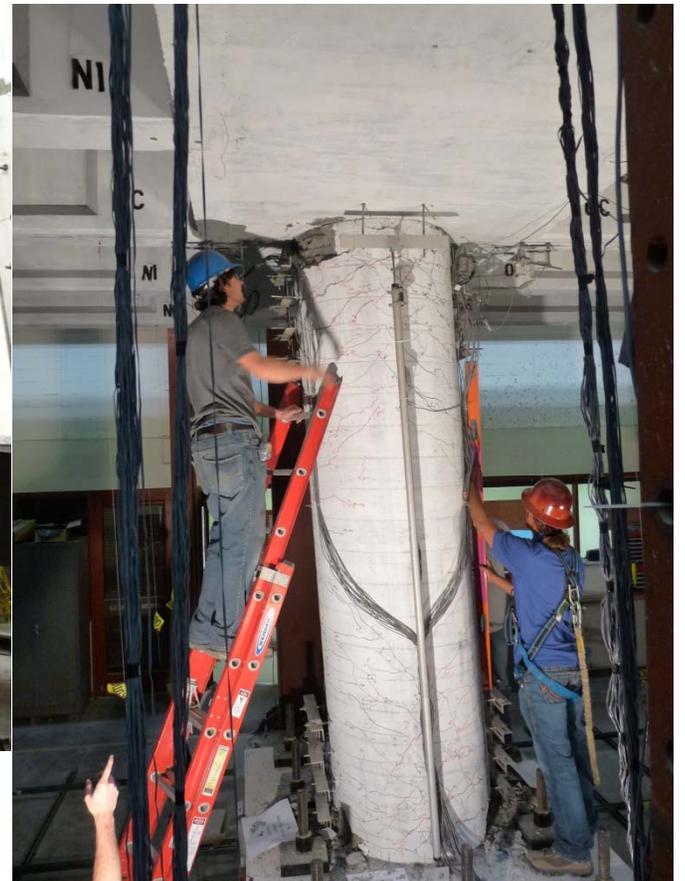
19



- ❑ Length of test unit was 66 ft
- ❑ Tie-downs and four vertical actuators simulated gravity effects
- ❑ Four horizontal actuators simulated the seismic action

# Phase I Configuration

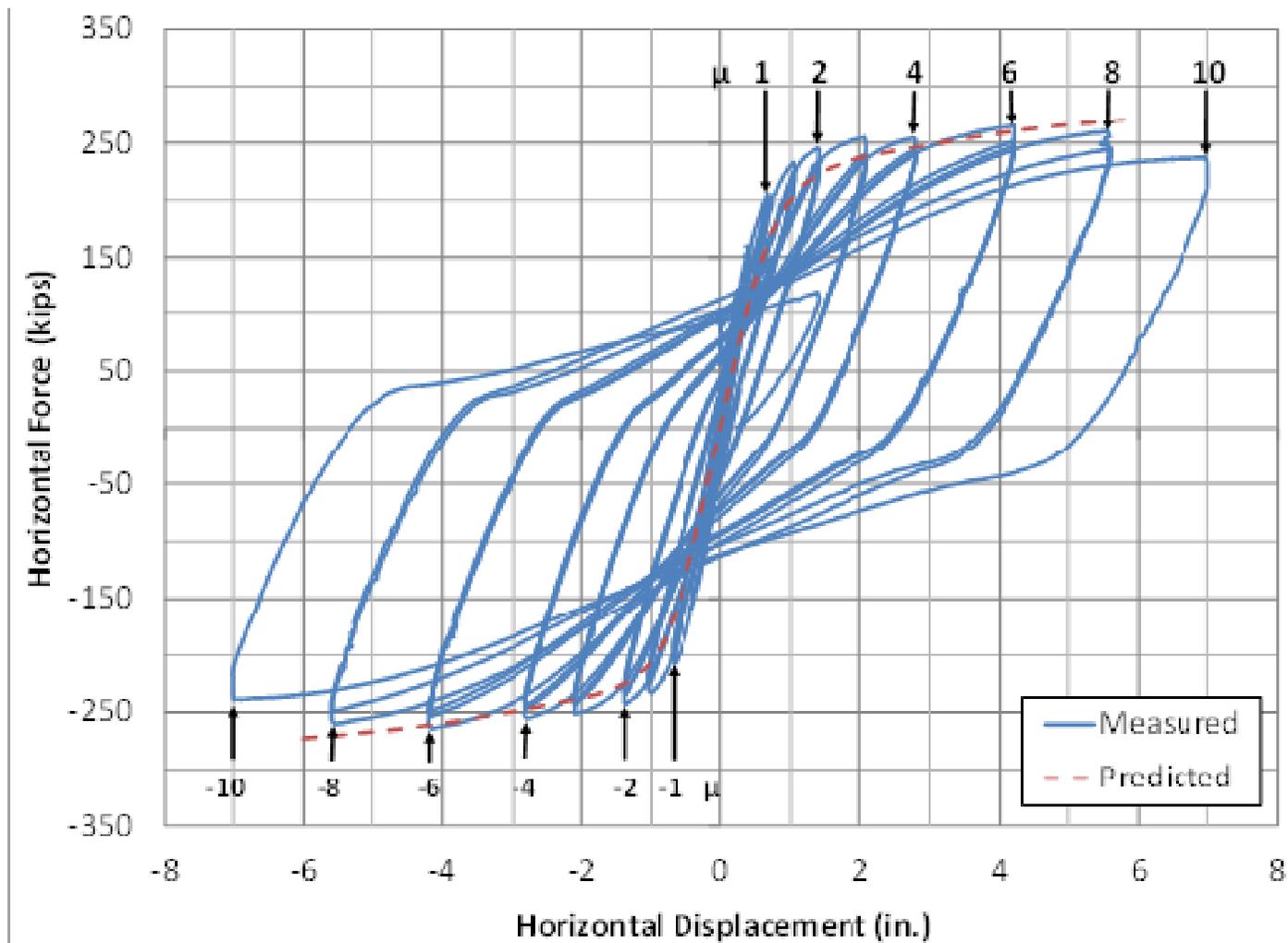
20



"Caltrans" "inverted tee"

# Force-Displacement Response

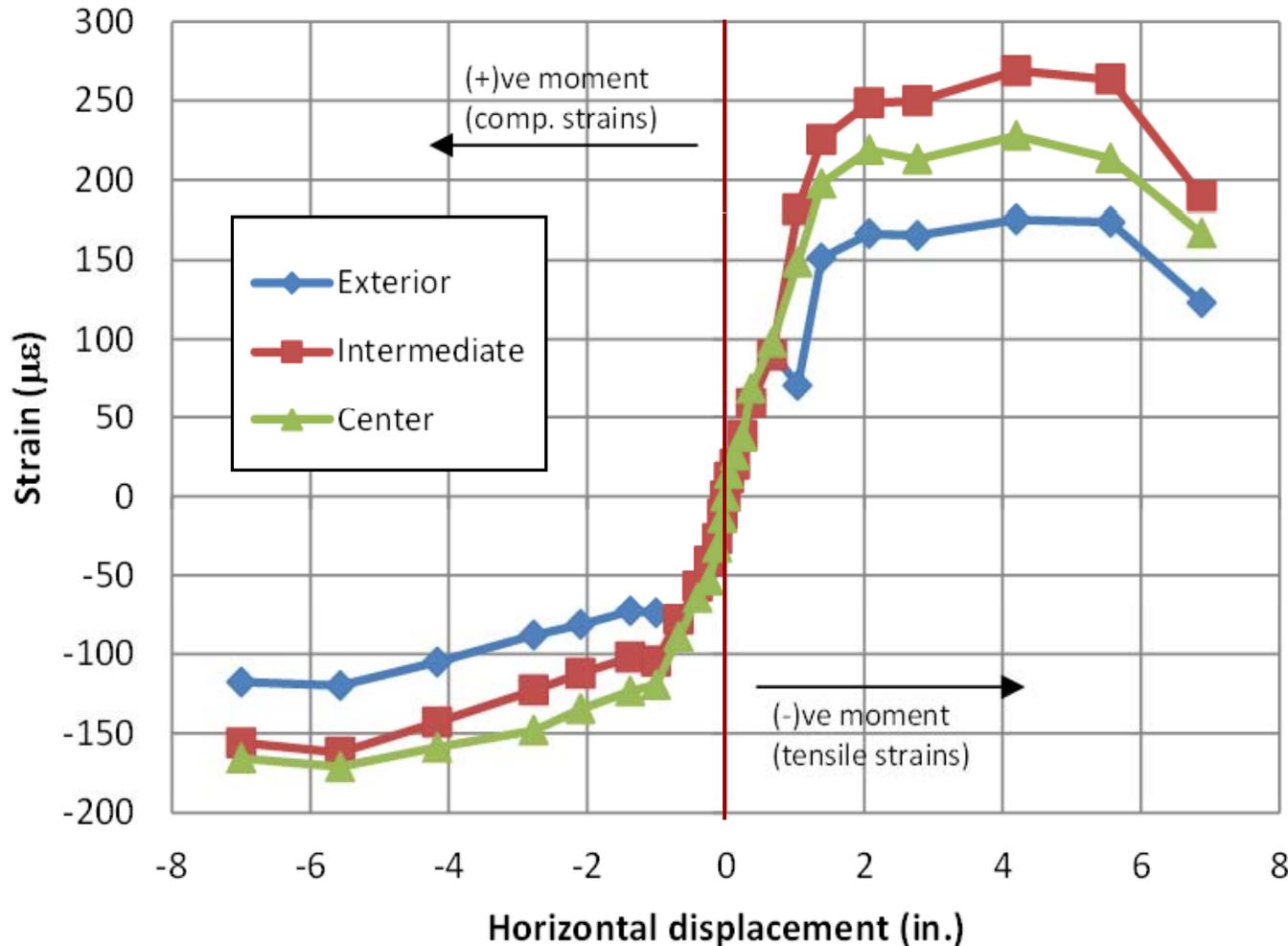
21



- Good comparison with SAP analysis
- Results converge as structure softens through cracking and yielding
- Similar behavior in both directions

# Girder Load Distribution (Improved Connection side)

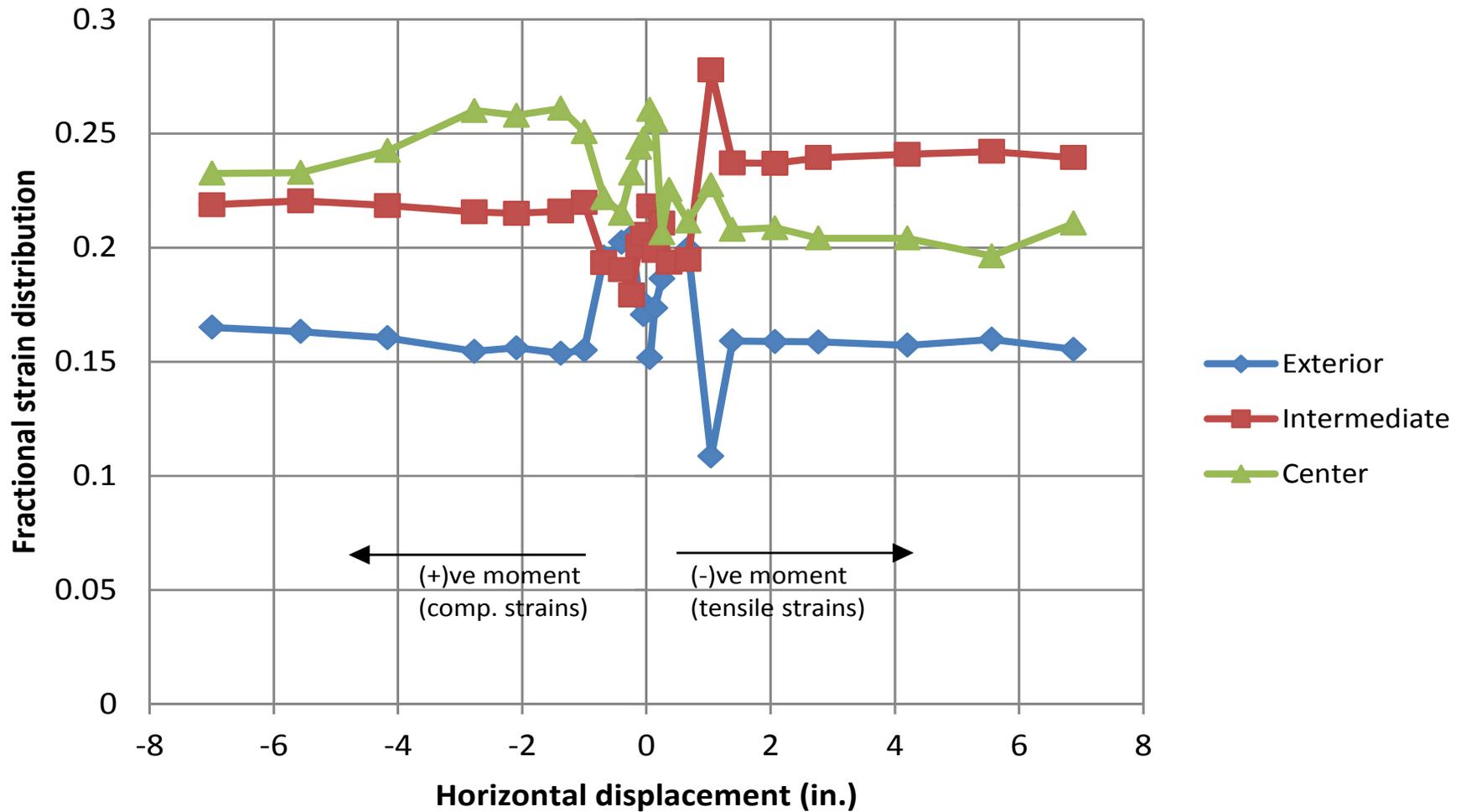
22



- Center: 20%
- Intermediate: 25%
- Exterior: 15%
- Compare to analysis: 22.8%
- 21.2%
- 17.4%

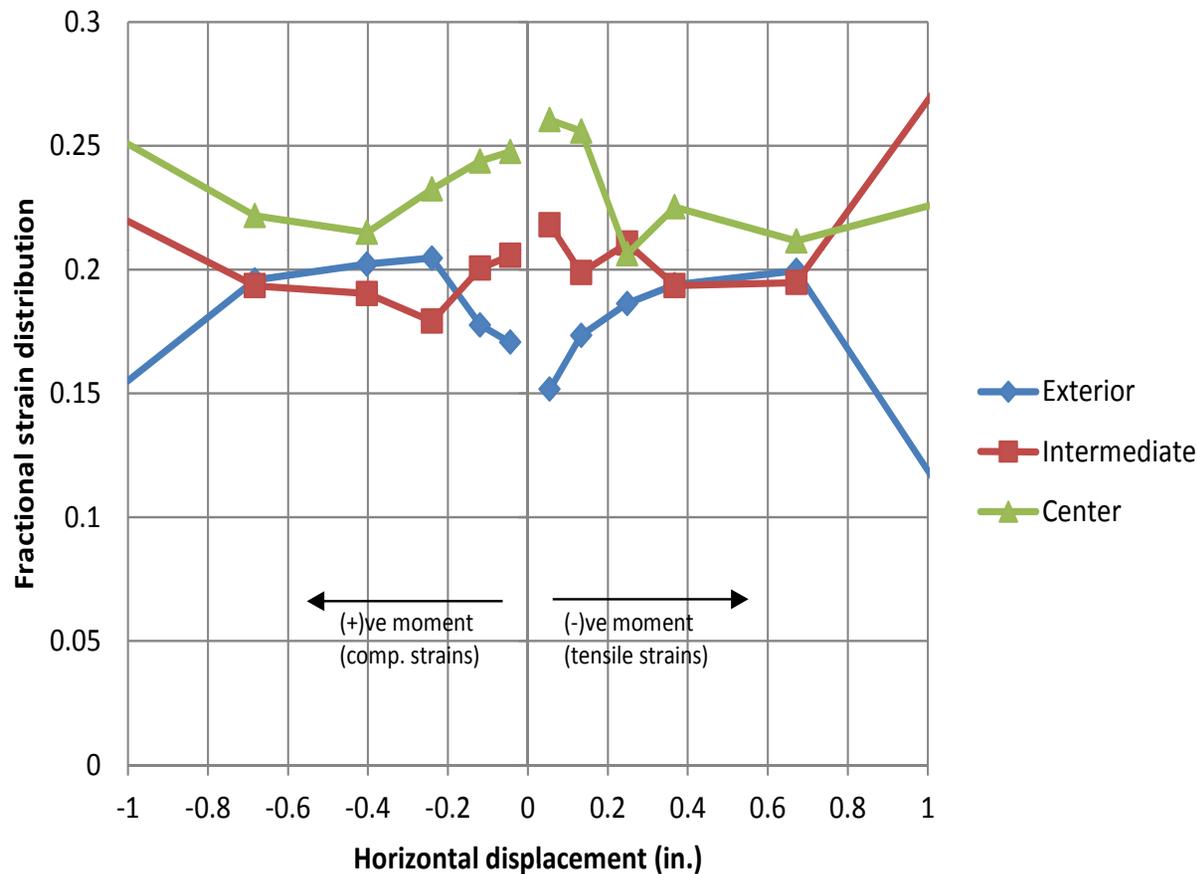
# Girder load distribution

23



# Girder load distribution (Low load levels)

24



- First step to right of zero corresponds to  $+0.25 F_y$
- Already significant load distribution occurring at this point
- Cen: 26.0%
- Int: 21.8%
- Ext: 15.1%

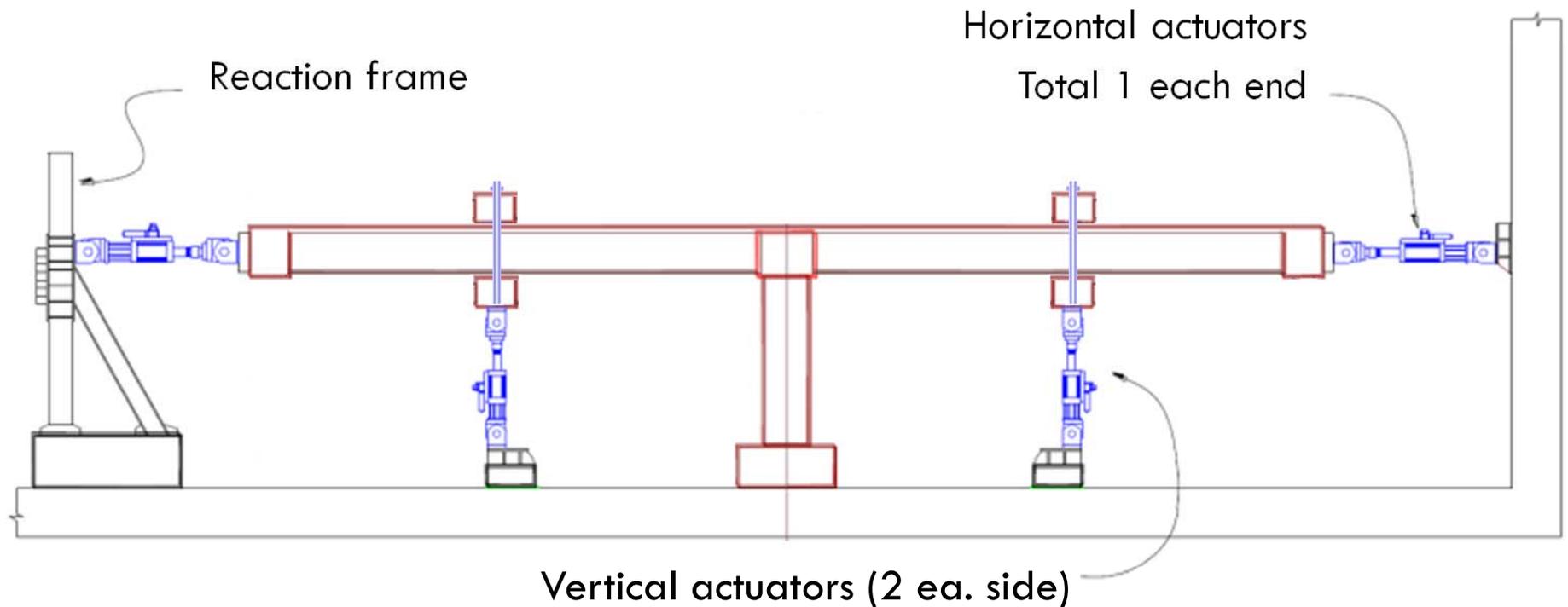
# Phase I General Performance

25

- Excellent overall performance for system and both as-built and improved connections
- Displacement ductility of 10 ( $\Delta_h = \pm 7$  in.)
- Little degradation of positive as-built connection (contrary to current design guides)
- Very little degradation to improved connection
- As-built connection: behaved as fixed; Minimal measures required to ensure satisfactory performance of existing inverted-tee – I-girder bridges

# Phase II Test Configuration

26



- ❑ Vertical load/displacement
- ❑ Full exercising of girder-to-cap connections
- ❑ Horizontal actuators – used for stability purposes

# Phase II Testing

27





# Phase II General Observations

29

- Maximum displacements:
  - ▣ Positive = 3 in. (upward)
  - ▣ Negative = 6 in. (downward)
- As-built connections exercised to full capacity
- Did not achieve full quantification of improved connection due to failure of the as-built connection and column hinges

# Phase II – As-built Connection Region

30



Opening up of as-built connection under positive-moment loading

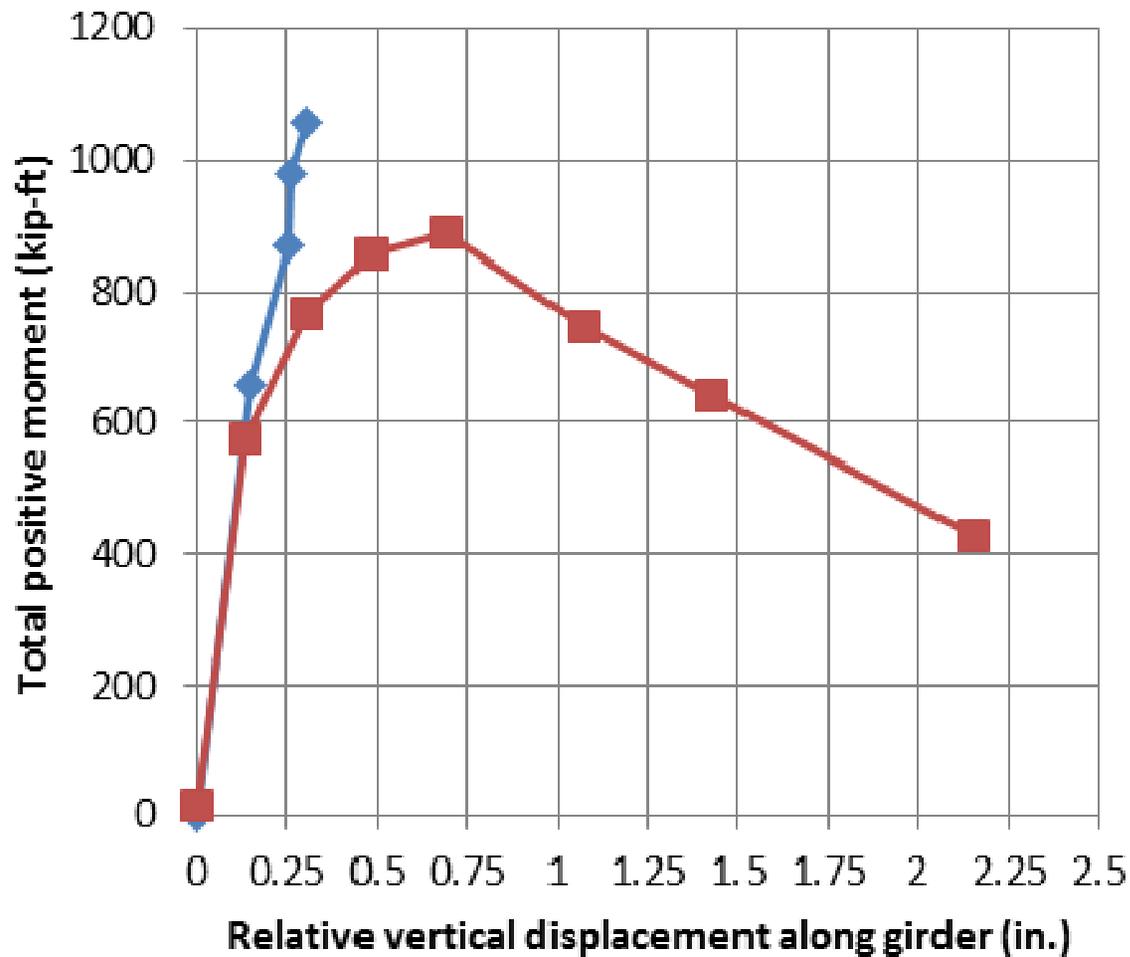
End of test



# Phase II

## Positive moment vs. displacement

31

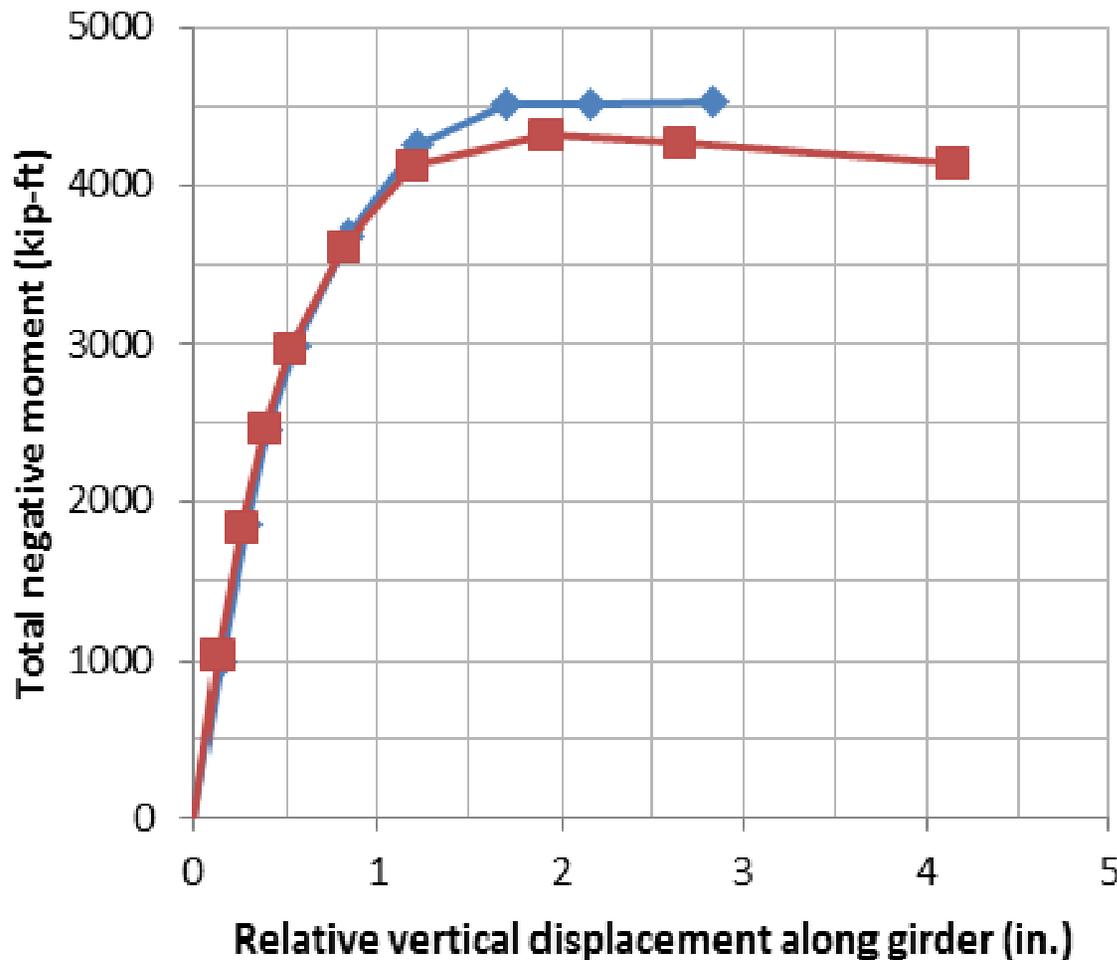


- Noticeable difference between improved and as-built
- Improved: elastic and higher moment
- Similar stiffness in elastic region

# Phase II

## Negative moment vs. displacement

32



- Difference more subtle
- Decrease in strength on as-built side
- Larger displacements for as-built side reflect the observed deterioration

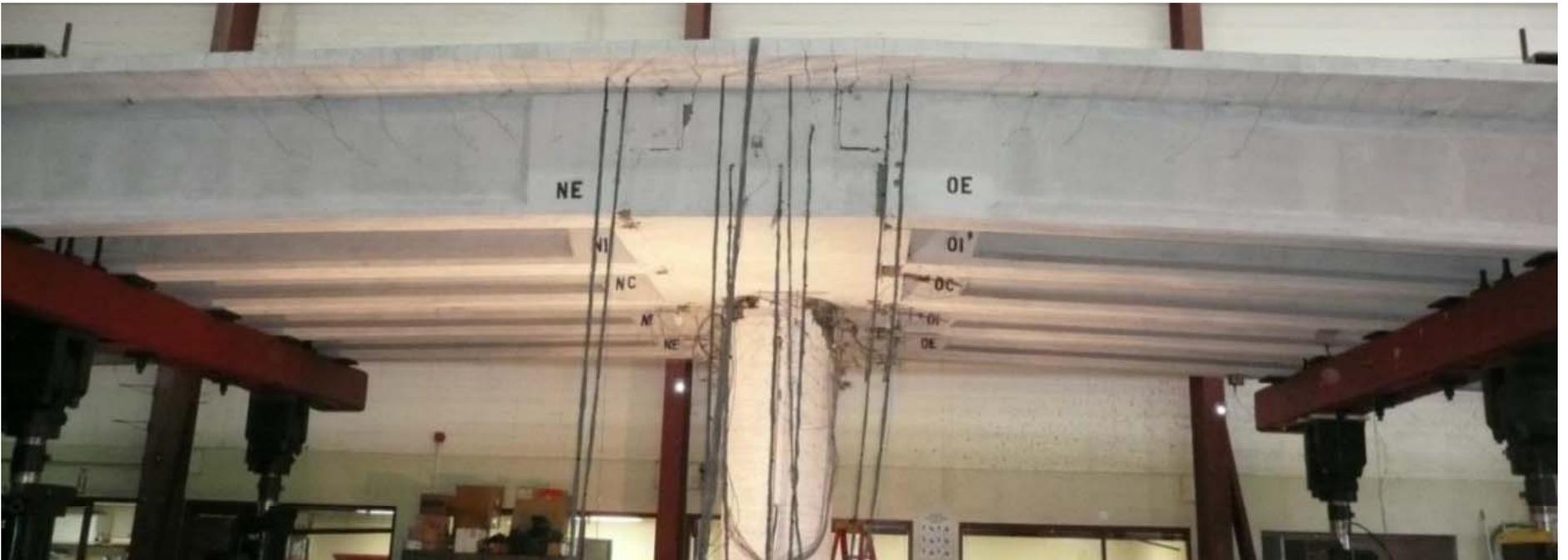
# Conclusions

33

- As-built connection behaved as a fully continuous connection during horizontal seismic testing, but this detail is not recommended for new bridges
- Only tops of columns in as-built bridges require retrofitting to prevent premature column damage, but note that
  - ▣ column shear demand will be increased
- Improved connection provided
  - ▣ dependable behavior under both positive and negative moments
  - ▣ an integral connection design to develop a plastic hinge in the top of the column
  - ▣ a means to promote ABC of bridges in seismic regions

# Thank You!

34



# Acknowledgements

35

- Caltrans (Mike Keever and Charly Sikorsky)
- Jay Holombo and Sami Megally of PBS&J
- Professor Jose Restrepo and the staff at UCSD and the Charles Lee Powell Laboratories