[LRFD Eq. 5.8.4.1-3]

[LRFD Art. 5.8.4.3

[LRFD Eq. 5.8.4.4-1]

[LRFD Eq. 5.8.4.1-4]

[LRFD Eq. 5.8.4.1-5]

BULB-TEE (BT-72), SINGLE SPAN, COMPOSITE DECK

9.1c.12.3 Required Interface Shear Reinforcement/9.1c.13 Minimum Longitudinal Reinforcement Requirement

 $V_{ni} = cA_{cv} + \mu(A_{vf}f_{vh} + P_c)$

where

- c = cohesion factor, ksi
- μ = coefficient of friction
- A_{cv} = area of concrete section resisting shear transfer, in.²
- A_{vf} = area of shear reinforcement crossing the shear plane, in.²
- P_c = permanent net compressive force normal to the shear plane, kips
- f_{yh} = specified yield strength of shear reinforcement, ksi

For cast-in-place concrete slabs placed on clean, concrete girder surface intentionally roughened:

c = 0.28 ksi

 $\mu = 1.0$

The actual contact width, b_{ν} , between the slab and the beam is 42 in.

 A_{cv} = (42.0 in.)(1.0 in.) = 42.0 in.²

LRFD Eq. 5.8.4.1-3 can be solved for A_{vf} as follows:

 $4.89 = 0.28(42.0) + 1.0(A_{vf}(60) + 0)$

Solving for *A*_{vf},

 A_{vf} (req'd) < 0

Since the resistance provided by cohesion is greater than the applied force, provide the minimum required interface reinforcement.

9.1c.12.3.1 Minimum Interface Shear Reinforcement

 $A_{vf} \geq (0.05A_{cv})/f_{yh}$

From the design of vertical shear reinforcement, a No. 4 double-leg bar at 12-in. spacing is provided from the beam extending into the deck. Therefore, $A_{vf} = 0.40$ in.²/ft

 $A_{vf} = 0.40 \text{ in.}^2/\text{ft}) < (0.05A_{cv})/f_{yh} = 0.05(42)/60 = 0.035 \text{ in.}^2/\text{in.} = 0.42 \text{ in.}^2/\text{ft}$ NG

However, LRFD Article 5.8.4.4 states that the minimum reinforcement need not exceed the amount needed to resist $1.33V_{hi}/\phi$ as determined using Eq. 5.8.4.1-3.

 $1.33(4.40/0.9) = 0.28(42.0) + 1.0(A_{vf}(60) + 0)$

solving for A_{vf} ,

 A_{vf} (req'd) < 0 OK

9.1c.12.4 Maximum Nominal Shear Resistance

 $V_{ni} \leq K_1 f_c' A_{cv}$ or $K_2 A_{cv}$

$$V_n$$
 provided = (0.28)(42) + 1.0 $\left(\frac{0.40}{12}(60) + 0\right)$ = 13.76 kips/in.

 $K_1 f'_c A_{cv} = (0.3)(4.0)(42) = 50.4$ kips/in.

 $K_2A_{cv} = 1.8(42) = 75.6$ kips/in.

Since provided $V_n = 13.76$ kips/in. < 50.4 kips/in. OK

9.1c.13 MINIMUM LONGITUDINAL REINFORCEMENT REQUIREMENT

See Section 9.1a.13. Although the values of V_s and $\cot \theta$ are slightly different in Example 9.1c.13, the calculations and end result are essentially the same.